Automatic differentiation of a fluid-structure interaction problem Gabriel Balaban, Anders Logg,

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Examples of Fluid-structure interaction





Modelling Challenges

- model must integrate solid and fluid mechanics
- fluid geometry depends on structure deformation

Solving the FSI problem

Issues:

- Continuum mechanics formulation
- Partitioned vs monolithic
- Fixed-pointed vs Newton
- Approximation of the Jacobian

In this work we:

- derive a Newton's method with exact Jacobians for FSI problems using the arbitrary Lagrangian Eulerian formulation
- implement a monolithic solver in Python (using FEniCS)
- investigate various optimizations and simplifications

Setup of the FSI problem



Mismatch in standard fluid and solid models



$$\rho_{F}(\dot{u}_{F} + \text{grad } u_{F} \cdot u_{F}) - \text{div } \sigma_{F} = b_{F}$$

div $u_{F} = 0$

Mesh smoothing problem





Mesh equation

$$\dot{D}_{_M} - \mathrm{Div} \ \Sigma_{_M}(D_{_M}) = 0$$

Arbitrary Lagrangian-Eulerian framework



ALE time derivative:

$$\frac{d}{dt}(\rho u) = \dot{\rho u} + \rho \left(\text{grad } u \cdot \left(u - \dot{D}_{M} \right) \right)$$

ALE fluid equation:

$$\begin{split} \rho_{\scriptscriptstyle F}(\dot{u}_{\scriptscriptstyle F} + \operatorname{grad} u_{\scriptscriptstyle F} \cdot (u_{\scriptscriptstyle F} - \dot{D}_{\scriptscriptstyle M})) - \operatorname{div} \sigma_{\scriptscriptstyle F}(u_{\scriptscriptstyle F}, p_{\scriptscriptstyle F}) &= b_{\scriptscriptstyle F} & \text{ in } \omega_{\scriptscriptstyle F}(t) \\ \operatorname{div} u_{\scriptscriptstyle F} &= 0 & \text{ in } \omega_{\scriptscriptstyle F}(t) \end{split}$$

Interface conditions



Stress continuity:

$$\sigma_{_{S}} \cdot \mathbf{n} = \sigma_{_{F}} \cdot \mathbf{n} \quad \text{ on } \gamma_{_{FS}}(t)$$

Kinematic continuity:

$$u_{\scriptscriptstyle F} = u_{\scriptscriptstyle S}$$
 on $\gamma_{\scriptscriptstyle FS}(t)$

Domain continuity:

$$d_{_M} = d_{_S}$$
 on $\gamma_{_{FS}}(t)$

Linearization of the FSI problem

Two challenges:

Derivative of fluid equation with respect to geometry?

$$\frac{d}{dt}(\rho u) - \operatorname{div} \sigma_F(u_F, p_F) = b_F \quad \text{in } \omega_F(t) \\ \operatorname{div} u_F = 0 \quad \text{in } \omega_F(t)$$

Linearization of essential BCs

$$egin{aligned} u_{\scriptscriptstyle F} &= u_{\scriptscriptstyle S} & ext{ on } \gamma_{\scriptscriptstyle FS}(t) \ d_{\scriptscriptstyle M} &= d_{\scriptscriptstyle S} & ext{ on } \gamma_{\scriptscriptstyle FS}(t) \end{aligned}$$

The reference domain approach



- Map the fluid problem to the reference domain
- Use standard techniques to differentiate
- Straightforward but tedious
- Can be automated!

Navier-Stokes pulled back to reference domain

Equation:

$$\begin{split} \rho_{\scriptscriptstyle F} J_{\scriptscriptstyle M}(\dot{U}_{\scriptscriptstyle F} + \operatorname{Grad} U_{\scriptscriptstyle F} \cdot F_{\scriptscriptstyle M}^{-1} \cdot (U_{\scriptscriptstyle F} - \dot{D}_{\scriptscriptstyle M})) - \operatorname{Div} \Sigma_{\scriptscriptstyle F} &= B_{\scriptscriptstyle F} \\ \operatorname{Div} (J_{\scriptscriptstyle M} F_{\scriptscriptstyle M}^{-1} \cdot U_{\scriptscriptstyle F}) &= 0 \end{split}$$

Pulled-back fluid stress:

$$\boldsymbol{\Sigma}_{\scriptscriptstyle F} = J_{\scriptscriptstyle M} \left(\boldsymbol{\mu}_{\scriptscriptstyle F}(\operatorname{Grad}\, \boldsymbol{U}_{\scriptscriptstyle F}\cdot \boldsymbol{F}_{\scriptscriptstyle M}^{-1} + \boldsymbol{F}_{\scriptscriptstyle M}^{-\top}\cdot \operatorname{Grad}\, \boldsymbol{U}_{\scriptscriptstyle F}^{\top}) - \boldsymbol{P}_{\scriptscriptstyle F}\boldsymbol{I} \right) \cdot \boldsymbol{F}_{\scriptscriptstyle M}^{-\top}$$

Interface conditions: How to linearize?



Stress continuity:

$$\Sigma_{_{S}} \cdot N = \Sigma_{_{F}} \cdot N \quad \text{ on } \Gamma_{_{FS}}$$

Kinematic continuity:

$$U_{_F} = U_{_S}$$
 on $\Gamma_{_{FS}}$

Domain continuity:

$$D_{_{M}} = D_{_{S}}$$
 on $\Gamma_{_{FS}}$

Linearization of essential boundary conditions

Introduce Lagrange multipliers ($\tau_{\rm F},\tau_{\rm M})$ and corresponding trial functions ($\chi_{\rm F},\chi_{\rm M})$

Kinematic continuity:

$$U_{\rm F} - U_{\rm S} \tau_{\rm F} \tau_{\rm FS} + \chi_{\rm F} v_{\rm F} \tau_{\rm FS}$$

Domain continuity:

$$D_{\rm M} - D_{\rm S} \tau_{\rm M} \Gamma_{\rm FS} + \chi_{\rm M} {\rm v}_{\rm M} \Gamma_{\rm FS}$$

The linearized FSI operator (the Jacobian)

 $R'^n(v,\delta U;U^n,U^{n-1})=$

$$\begin{split} & \left\{ v_{\mu}, \rho_{\mu} J_{\mu}^{0} (dD_{\mu}^{n} + \operatorname{Grad} \delta U_{\mu}^{n-1} + F_{\mu}^{-1,n} : (D_{\mu}^{n-1} - D_{\mu}^{n}) + \operatorname{Grad} U_{\mu}^{n-1} \cdot F_{\mu}^{-1,n} : (D_{\mu}^{n-1} - D_{\mu}^{n}) + \operatorname{Grad} U_{\mu}^{n-1} \cdot F_{\mu}^{-1,n} : (D_{\mu}^{n-1} - D_{\mu}^{n}) + \left\{ \operatorname{Grad} v_{\mu}, J_{\mu}^{0} (\operatorname{Grad} \delta U_{\mu}^{n-1} + F_{\mu}^{-1,n} : U_{\mu}^{n-1} \cdot U_{\mu}^{n-1} : (U_{\mu}^{n-1} - D_{\mu}^{n})) \right\}_{\mu} \\ & - \left(\operatorname{Grad} v_{\mu}, J_{\mu}^{0} (\operatorname{Grad} \delta D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : (D_{\mu}^{n-1} - D_{\mu}^{n})) \right)_{\mu} \\ & - \left(v_{\mu}, J_{\mu}^{0} (\operatorname{Grad} \delta D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : (U_{\mu}^{n-1} - D_{\mu}^{n})) \right)_{\mu} \\ & - \left(v_{\mu}, \rho_{\mu} J_{\mu}^{0} (\operatorname{Grad} \delta D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : (\operatorname{Grad} U_{\mu}^{n-1} - D_{\mu}^{n})) \right)_{\mu} \\ & - \left\langle v_{\mu}, \rho_{\mu} J_{\mu}^{0} (\operatorname{Grad} \delta D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : (\operatorname{Grad} U_{\mu}^{n-1} - D_{\mu}^{n}) \right)_{\mu} \\ & - \left\langle \operatorname{Grad} v_{\mu}, J_{\mu}^{0} (P_{\mu} \operatorname{Grad} d D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : \operatorname{Grad} d U_{\mu}^{n-1} - D_{\mu}^{n}) \right\rangle_{\mu} \\ & - \left\langle \operatorname{Grad} v_{\mu}, J_{\mu}^{0} (P_{\mu} \operatorname{Grad} D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : \operatorname{Grad} d D U_{\mu}^{n-1} - D_{\mu}^{n}) \right\rangle_{\mu} \\ & - \left\langle \operatorname{Grad} v_{\mu}, J_{\mu}^{0} (P_{\mu} \operatorname{Grad} D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : \operatorname{Grad} d D U_{\mu}^{n-1} - F_{\mu}^{-1,n} \right\rangle_{\mu} \\ & - \left\langle \operatorname{Grad} v_{\mu}, J_{\mu}^{0} (P_{\mu} \operatorname{Grad} D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : \operatorname{Grad} d D U_{\mu}^{n-1} + F_{\mu}^{-1,n} \right\rangle_{\mu} \\ & + \left\langle \operatorname{Grad} v_{\mu}, D U_{\mu} (P_{\mu} \operatorname{Grad} d D U_{\mu}^{n-1} + F_{\mu}^{-1,n} : \operatorname{Grad} d D U_{\mu}^{n-1} + F_{\mu}^{-1,n} \right\rangle_{\mu} \\ & + \left\langle \operatorname{Grad} v_{\mu}, D U_{\mu} (P_{\mu} \operatorname{Grad} d D U_{\mu}^{n-1} + V_{\mu}^{n-1} : \operatorname{Grad} d D U_{\mu}^{n-1} + V_{\mu} \\ & + \left\langle \operatorname{Grad} v_{\mu}, \operatorname{Grad} d D U_{\mu}^{n-1} : \left\langle \operatorname{Grad} \delta D_{\mu}^{n-1} + V_{\mu} \\ & + \left\langle \operatorname{Grad} v_{\mu}, U_{\mu} + \left\langle \operatorname{Grad} \delta U_{\mu}, U_{\mu} + V_{\mu} \\ & + \left\langle \operatorname{Grad} \delta U_{\mu} + U_{\mu}^{n-1} : \left\langle \operatorname{Grad} \delta D U_{\mu}^{n-1} + V_{\mu} \\ & + \left\langle \operatorname{Grad} \delta U_{\mu} + U_{\mu} \\ & + \left\langle \operatorname{Grad} \delta U_{\mu} + U_{\mu} \\ & + \left\langle \operatorname{Grad} \delta U_{\mu} \\$$



FEniCS implementation

J = derivative(R, U)

An analytic test problem

pdf/pdf/analyticproblem.pdf_tex Primary variables:

$$U_{F} = y(1 - y) \sin t$$

$$P_{F} = 2C \sin t (1 - x - Cxy(1 - y)(1 - \cos t))$$

$$D_{S} = Cy(1 - y)(1 - \cos t)$$

$$U_{S} = Cy(1 - y) \sin t$$

$$D_{M} = Cxy(1 - y)(1 - \cos t)$$

Convergence for analytic test problem



A two-dimensional blood vessel



Break-down of run-time

Problem	Routine	Calls	Time (s)	
Analytic problem	Jacobian assembly	28	83.9s	90%
mesh size $= 231$	Linear solve	28	1.86s	2%
time steps $= 10$	Residual assembly	38	0.915s	1%
Blood vessel	Jacobian assembly	343	2980s	81%
mesh size $= 1271$	Linear solve	343	254s	18%
time steps $= 140$	Residual assembly	483	64.1s	1%

Effect of Jacobian reuse

Problem	Routine	Calls	
Analytic problem	Jacobian assembly	1 (-27)	-95 %
mesh size $= 231$	Linear solve	51 (<mark>+23</mark>)	-96%
time steps $= 10$	Residual assembly	61 (<mark>+23</mark>)	+54%
	Total Runtime:		-93 %
Blood vessel	Jacobian assembly	25 (-308)	-93 %
mesh size $= 1271$	Linear solve	1287 (<mark>+944</mark>)	-92 %
time steps $= 140$	Residual assembly	1427 (<mark>+944</mark>)	+192%
	Total		-91 %

Effect of Jacobian reuse



Optimization summary

Optimization	Runtime	Memory	Robustness
Jacobian Reuse		<u>f</u>	<u>for</u>
Jacobian Simplification	<u>e</u>		
Jacobian Buffering			<u>e</u>
Reduced Quadrature Order		<u>f</u>	

Summary: How to use the automatic derivative to solve FSI problems

- Map the fluid equation to the reference domain
- Impose essential BC's using Lagrange multipliers
- Let the automatic derivative compute the Jacobian

Challenges / work in progress:

- Long FFC compilation times
- Preconditioning

